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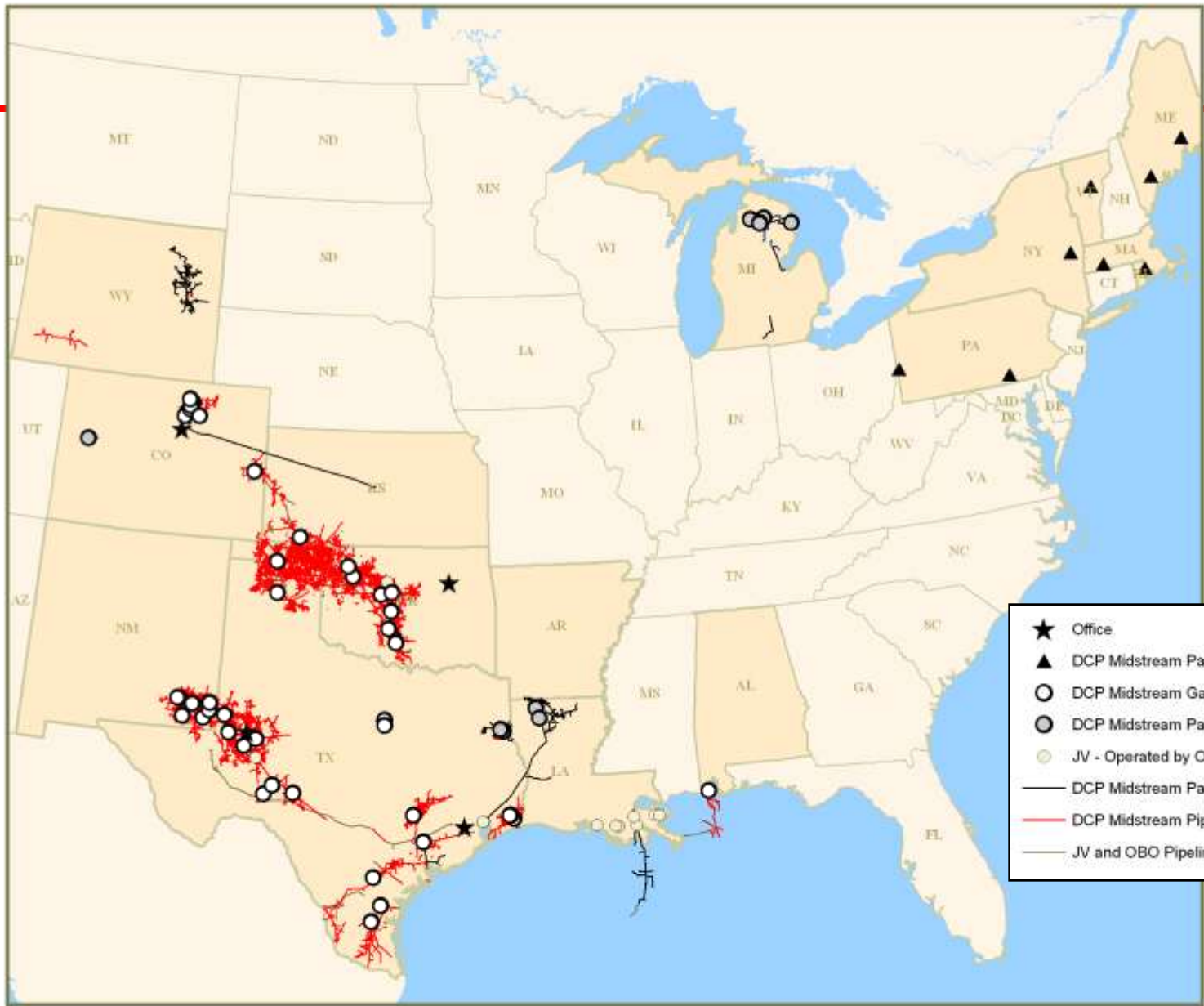
# **Determining Remaining Strength of Corroded Pipelines**

**Houston Section  
April 10, 2012**

# Who is DCP Midstream?

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- Formerly *Duke Energy Field Services* the Company was renamed on January 1, 2007 to align with DCP Midstream Partners.
- DCP Midstream, LLC is a private company. A 50-50 joint venture between Spectra Energy and ConocoPhillips.
- One of the nation's largest natural gas gatherers and processors (7 Bcf/day), the largest natural gas liquids (NGLs) producer and one of the largest NGL marketers in the U.S.
- Operates in 26 states, gathers raw natural gas through ~62,000 miles of pipe and processes gas through 61 plants, produces 360,000 bbls/day NGLs
- Over 3,000 employees



- ★ Office
- ▲ DCP Midstream Partners Propane Terminal
- DCP Midstream Gas Plant
- DCP Midstream Partners Gas Plant
- ◐ JV - Operated by Other Facility
- DCP Midstream Partners Pipeline
- DCP Midstream Pipeline
- JV and OBO Pipelines

# Introduction

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- Pipeline Design
- ASME B31G
- Limits for B31G
- Misc

# Pipeline Design

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Barlow's formula relates pressure to pipe attributes

$$P = 2 S t / D$$

- P = Design pressure
- S = Yield strength in psi
- D = Outside diameter
- t = Nominal wall thickness

# Pipeline Design

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- Barlow's formula
- $P = (2 St/D) \times F \times E \times T$

P = Design pressure

S = Yield strength in psi

D = Outside diameter

t = Nominal wall thickness

F = Design factor

E = Longitudinal joint factor

T = Temperature derating factor...

# Peter Barlow

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## Peter Barlow

### Peter Barlow

Self-educated, Peter Barlow (1776-1862) became assistant mathematics master at the Royal Military Academy, Woolwich, in 1801. He published numerous mathematical works, including *New Mathematical Tables* (1814). Later known as *Barlow's Tables*, this compilation of factors and functions of all numbers from 1 to 10,000 was considered so accurate and so useful that it has been regularly reprinted ever since.



Woolwich -SE of London. Active 1741–1939

# Pipeline Design

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## Design factor (F)

- Liquid Pipelines 0.72
- Gas Pipelines
  - Class 1 0.72
  - Class 2 0.60
  - Class 3 0.50
  - Class 4 0.40



# Pipeline Design

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Example: Liquid line

6" .219 wt X42

$$P = (2 \times 42000 \times .219 / 6.625)$$

$$P = 2777 \text{ psi}$$

$$P_{\text{max mop}} = 2777 \text{ psi} \times .72 = 1999$$

# ASME B31G

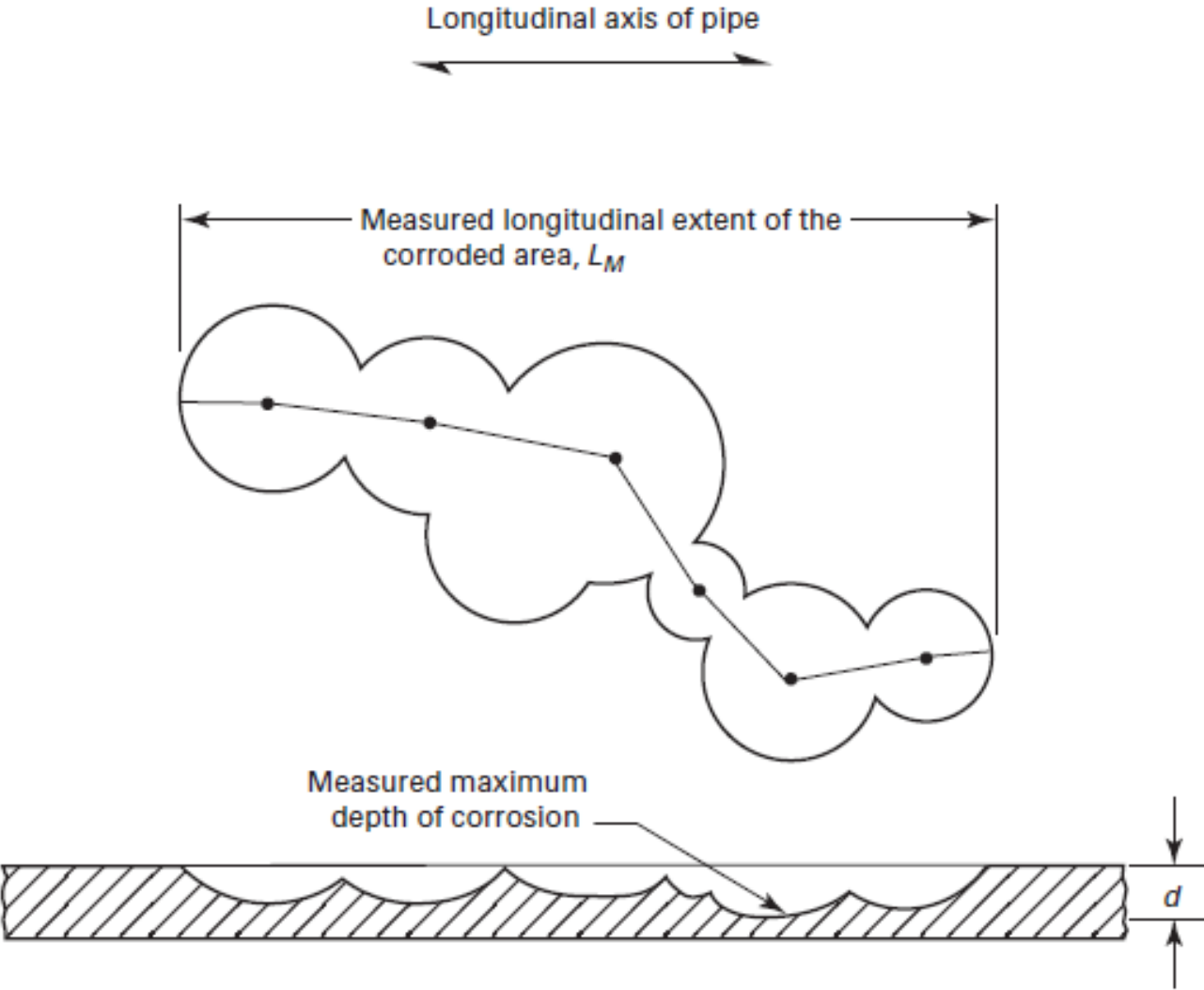
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A supplement to ASME B31

Calculates Burst pressure with pipe parameters  
and metal loss >>

- Length - L
- depth - d

# ASME B31G



# ASME B31G

## Corroded Pipe Assessment

### Failure Criterion

$$\sigma_{\text{Failure}} = \bar{\sigma} \left[ \frac{1 - \frac{A}{A_0}}{1 - \frac{A}{A_0} M^{-1}} \right]$$

Where:

$\sigma_{\text{Failure}}$	Predicted Failure Stress
$\bar{\sigma}$	Flow Stress, f{SMYS}
A	Effective Area of Missing Metal
$A_0$	Original Area, {L x t}
M	Folias Factor, f{L, D, t}
L	Effective Length

# ASME B31G

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## Folias Factor

$$\text{For } L \leq \sqrt{50Dt}, M = \sqrt{1 + 0.6275 \frac{L^2}{Dt} - 0.003375 \left(\frac{L^2}{Dt}\right)^2}$$

$$\text{For } L > \sqrt{50Dt}, M = 0.032 \frac{L^2}{Dt} + 3.3$$

# ASME B31G

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- Based on Battelle Institute work July 1971
- ASME Guide
- ASME B31G - 1984
- Modified B31G - 1991
- Current edition B31G-2009

# ASME B31G

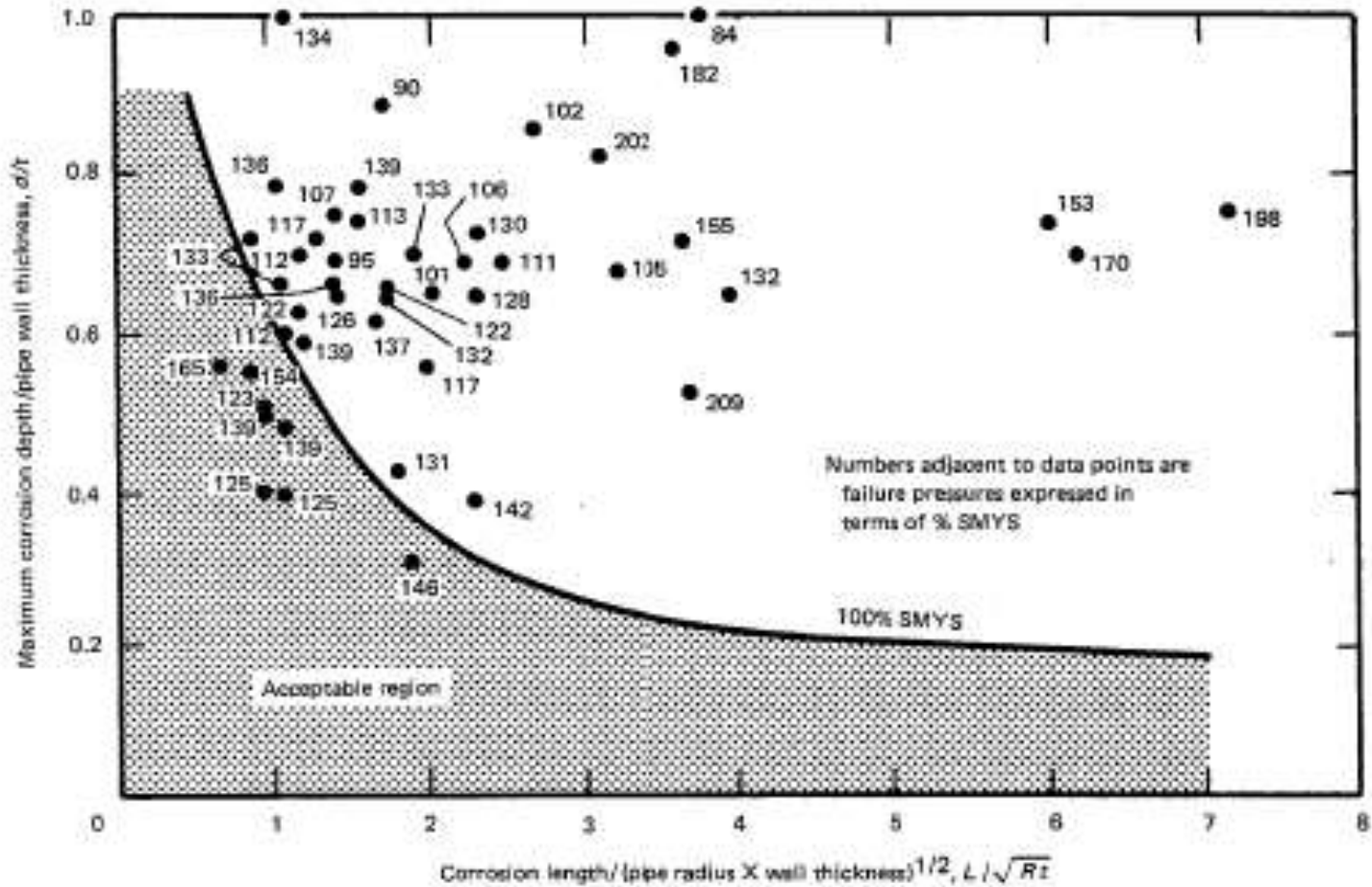


FIG. 1-1 PARABOLIC CRITERIA FOR CLASSIFYING CORROSION DEFECTS ACCORDING TO PREDICTED FAILURE STRESS

# ASME B31G

Equations are empirical or in some cases semi-empirical.

## What is this?

Empirical knowledge comes from observation only. You don't know why or have any idea of why reaction A follows situation B but you have seen it happen so many times that you KNOW that is what is going to happen.

People knew that things fell down long before there was a theory of gravitation. Such knowledge was empirical.

Empirical knowledge not only comes from observation but also by testing.

Read more: cp

[http://wiki.answers.com/Q/What\\_is\\_empirical\\_knowledge#ixzz1rfG](http://wiki.answers.com/Q/What_is_empirical_knowledge#ixzz1rfG)  
[SpoND](#)



# ASME B31G

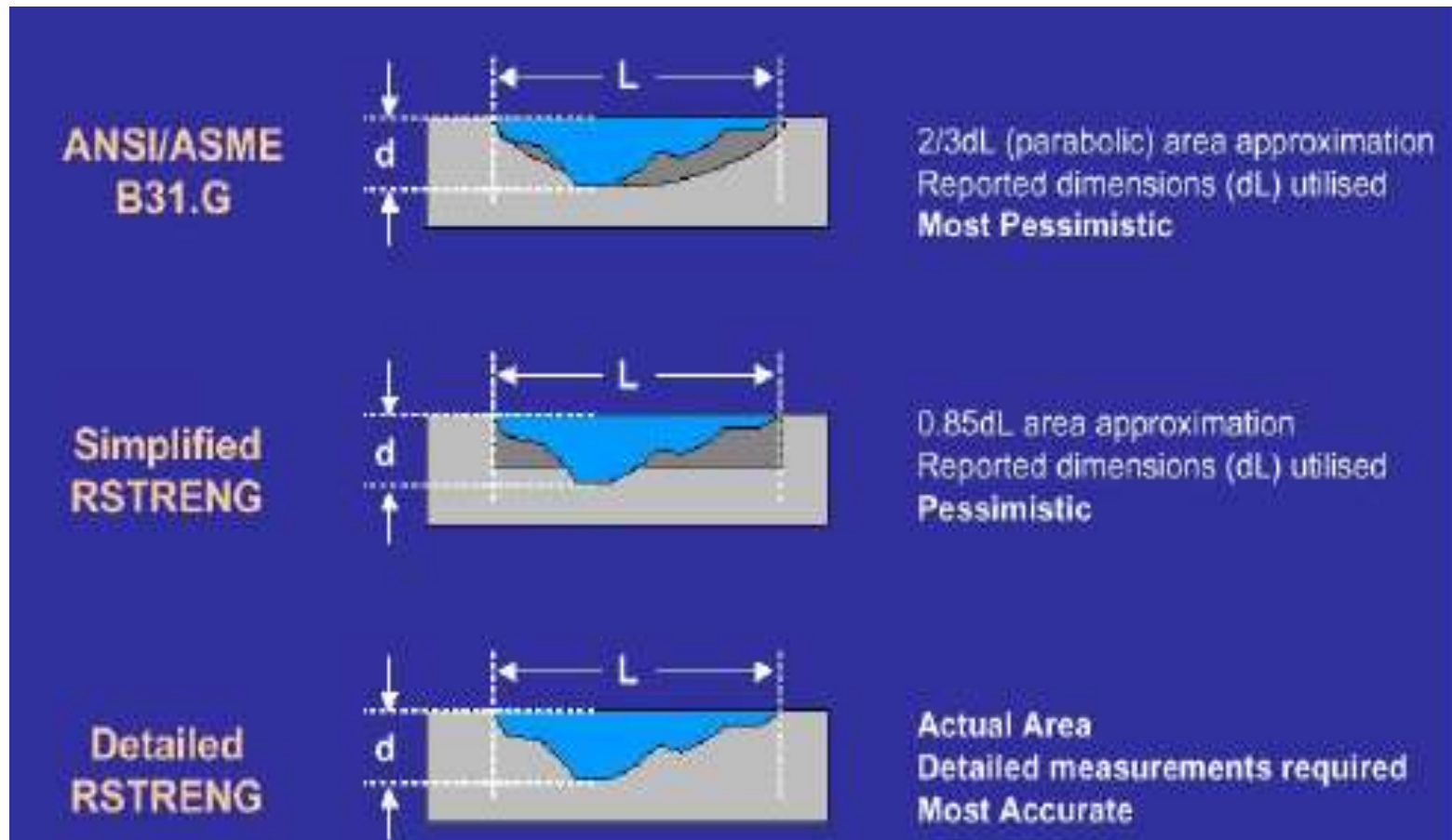
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3 versions

- ASME B31G
- Modified B31G
- Effective Area Method

# ASME B31.G

## Difference in methods



# ASME B31G

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## Application

- Yes for blunt metal loss
- Yes for external corrosion
- Yes for internal corrosion

# ASME B31G

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## Limitations (RULES)

- Depth less than 80% wt
- **No Cracks**
- **No gouges**
- **No stress Concentrator**
- **No selective seam corrosion**
- **No selective weld corrosion**
- Apply operating characteristics  $P_{\text{safe}}$

# ASME B31G

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In operations, always

- Identify cause of metal loss
- Mitigate cause of metal loss

# B31G

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- Company Operating Manuals
- KAPA (“KAPA” is an acronym for “Kiefner & Associates Pipe Assessment”)
- RSTRENG®

# B31G



# B31 G Interaction

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Interaction rule

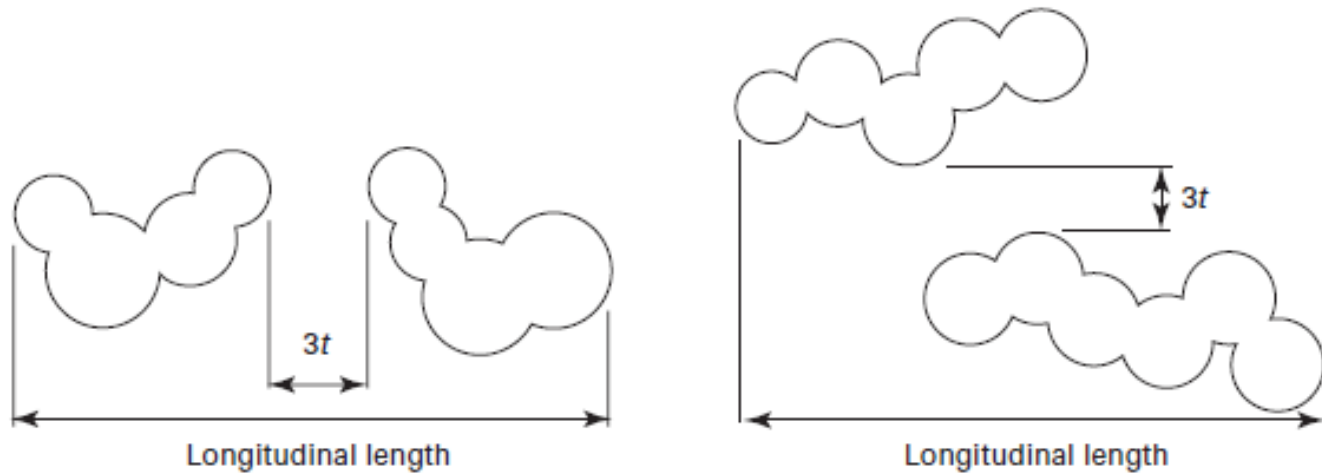
Commonly used **1" x 6t interaction**

- 1 inch in axial length separation
- 6 times pipe wall thickness for width separation (.250 wt = 1.5 in)
- If separation < 1" x 6t group or cluster the anomalies together.



# Interaction B31G

Fig. 1.12-1 Corrosion Pit Interaction Distances



# B31G



# B31G



# ASME B31G

Table 3-2 Values of  $L$  for Pipe Sizes  $\geq$  NPS 6 and  $<$  NPS 10

Depth, $d$ , in.	Wall Thickness, $t$ , in.							
	0.083	0.125	0.156	0.188	0.203	0.219	0.250	0.312
0.01	3.32	No limit	No limit	No limit	No limit	No limit	No limit	No limit
0.02	1.53	4.08	4.55	3.83	No limit	No limit	No limit	No limit
0.03	0.88	1.89	3.37	5.00	5.20	5.40	5.77	No limit
0.04	0.65	1.25	1.90	2.91	3.61	4.65	5.77	6.44
0.05	0.51	0.97	1.40	1.97	2.30	2.73	3.86	6.44
0.06	0.42	0.80	1.13	1.54	1.77	2.04	2.67	4.77
0.07	...	0.68	0.96	1.29	1.46	1.66	2.11	3.37
0.08	...	0.59	0.83	1.11	1.25	1.42	1.77	2.68
0.09	...	0.52	0.74	0.98	1.10	1.24	1.54	2.26
0.10	...	0.46	0.66	0.88	0.99	1.11	1.37	1.97
0.11	...	...	0.59	0.80	0.90	1.01	1.24	1.76
0.12	...	...	0.54	0.73	0.82	0.92	1.13	1.60
0.13	...	...	...	0.66	0.75	0.85	1.04	1.46
0.14	...	...	...	0.61	0.69	0.78	0.96	1.35
0.15	...	...	...	0.56	0.64	0.72	0.89	1.26
0.16	...	...	...	...	0.59	0.67	0.83	1.18
0.17	...	...	...	...	...	0.63	0.78	1.10
0.18	...	...	...	...	...	...	0.73	1.04
0.19	...	...	...	...	...	...	0.69	0.98
0.20	...	...	...	...	...	...	0.65	0.93
0.21	...	...	...	...	...	...	...	0.88
0.22	...	...	...	...	...	...	...	0.84
0.23	...	...	...	...	...	...	...	0.80
0.24	...	...	...	...	...	...	...	0.76

# ASME B31G

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Since  $L > 15/16''$  must repair

What about Modified B31G?

# Links and Reference

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<http://www.kiefner.com/downloads.asp>

<http://www.ttoolbox.com/Products/>

Duane Cronin

<https://uwspace.uwaterloo.ca/bitstream/10012/478/1/NQ51187.pdf>



**Kiefner & Associates, Inc.**  
 585 Scherers Court  
 Worthington, Ohio 43085  
 Phone (614) 888-8220 | Fax (614) 888-7323  
[www.kiefner.com](http://www.kiefner.com)

V050125

Diameter 6.625 Inches  
 Wt 0.219 Inches  
 SMYS 42,000 psi  
 MOP 1440 psi  
 CVN 20 ft-lb  
 Design Factor 0.72  
 Percent Operating Stress 51.9%  
 Maximum Allowable Pressure 1,999.3 psi

US Customary  
 Metric

Line Number N-1  
 Station Number 236+45  
 Mile Post 4.5

		Envelope Default Profile	Grid 1										
Effective Area Method	Predicted Failure Pressure (P <sub>f</sub> )	2867.7	2867.7										
	Factor of Safety (P <sub>f</sub> /MOP)	1.99	1.99										
Modified B31G	Predicted Failure Pressure (P <sub>f</sub> )	3007.8	3007.8										
	Factor of Safety (P <sub>f</sub> /MOP)	2.09	2.09										
B31G	Predicted Failure Pressure (P <sub>f</sub> )	2743.8	2743.8										
	Factor of Safety (P <sub>f</sub> /MOP)	1.91	1.91										
Calculated Parameters	Total Length	1.00	1.00										
	Eff. length	1.00	1.00										
	Start Length	0.00	0.00										
	Stop Length	1.00	1.00										
	Max PR Depth	0.120	0.120										
	Max. Depth/Thick	0.548	0.548										
	Eff. Area	0.12	0.12										

Released: April 28, 2009

# Kapa

V050125



**Kiefner & Associates, Inc.**  
 585 Scherers Court  
 Worthington, Ohio 43085  
 Phone (614) 888-8220 | Fax (614) 888-7323  
[www.kiefner.com](http://www.kiefner.com)

Diameter 6.625 inches  
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US Customary  
 Metric

Line Number N-1  
 Station Number 236+45  
 Mile Post 4.5

Area Code	Predicted Failure Pressure (P <sub>f</sub> )	Envelope Defect Profile										
		Grid 1										
	2867.7	2867.7										



# Kapa p2

		Envelope Defect Profile	Grid 1									
Effective Area Method	Predicted Failure Pressure (P <sub>f</sub> )	2867.7	2867.7									
	Factor of Safety (P <sub>f</sub> /MOP)	1.99	1.99									
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# Limits for B31G

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- Depth less than 80% wt
- Apply operating characteristics  $P_{safe}$
- **No Cracks**
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- **No stress Concentrator**
- **No selective seam corrosion**
- **No selective weld corrosion**

# Limits for B31G

OK for blunt metal loss

- Internal Corrosion
- External Corrosion
- Welds if metal loss not selective

**Must stop cause of metal loss – remember identify the cause, and fix**

# ILI spreadsheets -example B31G calcs

EVENT LOCATION				ANOMALY DESCRIPTION				ANOMALY REPAIR FACTORS			
EVENT	WHEEL COUNT (ft.)	DIST FROM U/S WELD (ft.)	DIST TO D/S WELD (ft.)	CLOCK	DEPTH %	LENGTH (in.)	INT / EXT	W.T (in.)	CALC. PFAIL .85dl (psi)	CALC. PFAIL .85dl / MAOP	COMMENTS
Anomaly	103397.81	27.42	30.81	1:50	50	22.9	I	0.17	990	1.16	
Anomaly	111302.51	32.43	30.94	1:00	54	10.3	I	0.175	989	1.16	
Girth Weld ID	Relative Distance (ft)	Absolute Distance (ft)	Comments	Peak Depth (%)	Length (in)	Width (in)	Local Wall Thickness (in)	SMYS (psi)	RESTRENGTH Burst (psi)	Orientation (clock)	Orientation (Degrees)
	19.51	211,621.20	Metal Loss EXTERNA	41%	7.86	1.39	0.250	42000	1509	5:30	195
	20.61	211,622.30	Metal Loss EXTERNA	39%	10.06	2.84	0.250	42000	1538	5:45	171
Pipeline Feature	INT/ EXT	Odometer (ft)	W. T.	Pipe Grade	Depth (%)	Depth (in.)	Length (in.)	Width (in.)	O'Clock Orientation	Burst Pressure (psi)	ERF
Metal Loss	EXT	519.01	0.312	X52	40%	0.125	0.8	0.6	3:00	2965	1.165
Metal Loss	EXT	523.04	0.312	X52	36%	0.112	0.6	0.6	3:31	2999	1.179











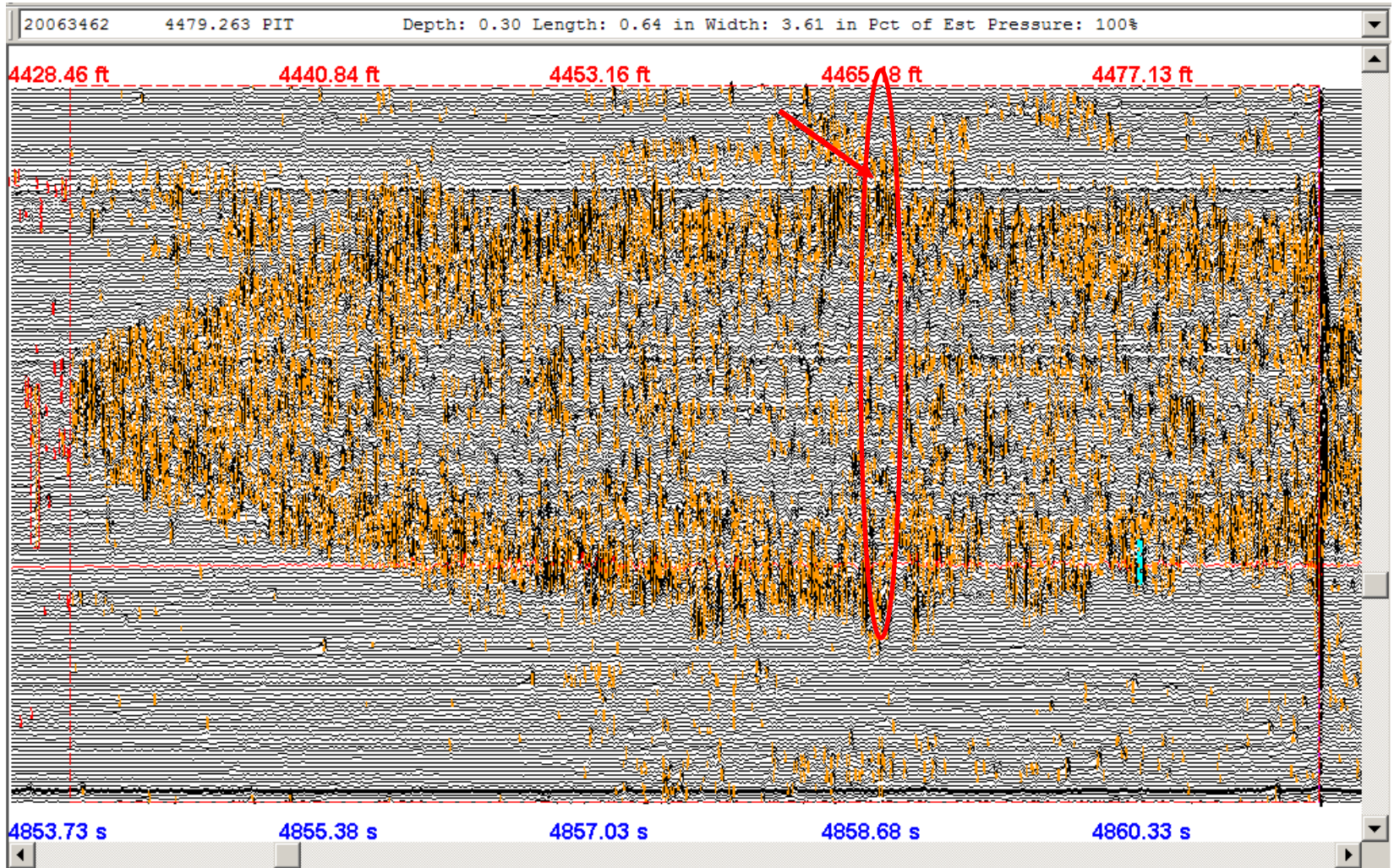








# Test Section 3 bottom view, typical pitting 20-40 %







25 DEGREES  
TOP OF PIPE

